

# Linear analyses of Runge-Kutta IMEX schemes for use in global atmospheric models

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with thanks to T. Allen, A. Staniforth, D. Durran

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- Motivation:
  - “**Gung-Ho**”: operational weather & climate forecasting model capable of exploiting  $O(10^5)+$  processors
  - For a semi-implicit model, from E. Mueller’s talk:
    - ⇒ very fast solution of very large decomposed elliptic problems
  - What do we do if the solvers can’t deliver within the forecast slot?
- Framework for numerical analyses of **R**unge-**K**utta **I**Mplicit-**E**Xplicit methods
- Summary of stability properties for several RK IMEX schemes
- Results from a numerical experiment: non-linear test case (Durran and Blossey, 2012)
- Comments

Consider linearized “compressible Boussinesq system” (Durrán and Blossey, 2012)

$$\begin{aligned} \left( \frac{\partial}{\partial t} + U \frac{\partial}{\partial x} \right) u + \frac{\partial P}{\partial x} &= 0 \\ \left( \frac{\partial}{\partial t} + U \frac{\partial}{\partial x} \right) w + \frac{\partial P}{\partial z} &= b \\ \left( \frac{\partial}{\partial t} + U \frac{\partial}{\partial x} \right) b + N^2 w &= 0 \\ \left( \frac{\partial}{\partial t} + U \frac{\partial}{\partial x} \right) P + c_s^2 \left( \frac{\partial u}{\partial x} + \frac{\partial w}{\partial z} \right) &= 0 \end{aligned}$$

where  $U$  is constant mean windspeed,  $c_s$  is speed of sound,

$$b = -g \frac{\rho - \bar{\rho}(z)}{\rho_0}, \quad P = \frac{p - \bar{p}(z)}{\rho_0}, \quad N^2 = -\frac{g}{\rho_0} \frac{d\bar{\rho}}{dz}$$

Yields dispersion relations:

$$(\omega - k_x U)^2 = \frac{c_s^2}{2} \left\{ k_x^2 + k_z^2 + \frac{N^2}{c_s^2} \pm \left[ \left( k_x^2 + k_z^2 + \frac{N^2}{c_s^2} \right)^2 - \frac{4N^2 k_x^2}{c_s^2} \right]^{1/2} \right\}$$

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For a **H**orizontally-**E**xplicit **V**ertically-**I**mplicit (HEVI) time-integration scheme,  
 consider largest horizontal and vertical Courant numbers:

$$C_x = c_s k_x \Delta t \quad C_z = c_s k_z \Delta t$$

Horizontal component defines a non-dimensional time-step that resolves  $c_s$  over  $\Delta x$ :

$$\Delta t^* = \max \{ C_x \} = c_s \max \{ k_x \} \Delta t \in [0, 2.5]$$

Then, the associated resolution of the vertical component can be described by

$$\frac{C_z}{\Delta t^*} = \frac{k_z}{\max \{ k_x \}}$$

For global weather/climate, what is  $\frac{C_z}{\Delta t^*} = \frac{k_z}{\max\{k_x\}} ?$

Horizontal mesh-spacings vary across applications:

$$\Delta x = \begin{cases} 10^3 \text{ m, for Gung - Ho weather} \\ 10^4 \text{ m, for UM weather} \\ 10^5 \text{ m, for global climate,} \end{cases}$$

Vertical mesh-spacings vary within a model:

$$\Delta z = \Delta z_B \dots \Delta z_T = 10 \dots 10^3 \text{ m}$$

Then,

$$\max\left\{\frac{C_z}{\Delta t^*}\right\} = \frac{\max\{k_z\}}{\max\{k_x\}} = \frac{\Delta x}{\Delta z_B} = \begin{cases} 10^2 \\ 10^3 \\ 10^4 \end{cases}, \quad \min\left\{\frac{C_z}{\Delta t^*}\right\} = \frac{\Delta x}{z_T} = \begin{cases} 10^{-2} \\ 10^{-1} \\ 10^0 \end{cases}$$

⇒ For our linear analyses, we will consider schemes' performance over

$$\Delta t^* \in [0, 2.5], \quad \frac{k_z}{\max\{k_x\}} \in [10^{-2}, 10^4]$$

For the linear stability analysis, we (further) simplify the system to

- 1 an ODE with fast and slow wave contributions:

$$F_t = -iK_H F - iK_V F,$$

where  $K_H = K_H(k_x)$  and  $K_V = K_V(k_z)$ ;

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- ② a system of horizontally & vertically propagating acoustic waves:

$$\begin{aligned} \frac{\partial u}{\partial t} + \frac{\partial P}{\partial x} &= 0 \\ \frac{\partial w}{\partial t} + \frac{\partial P}{\partial z} &= 0 \\ \frac{\partial P}{\partial t} + c_s^2 \left( \frac{\partial u}{\partial x} + \frac{\partial w}{\partial z} \right) &= 0 \end{aligned}$$

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"UFPReB" (**U**-Forward **P**-Backward)

The  $\nu$ -stage RK IMEX scheme that steps system

$$\mathbf{y}_t = \mathbf{s}(\mathbf{y}, t) + \mathbf{f}(\mathbf{y}, t),$$

from time  $t = n\Delta t$  to  $t = (n + 1)\Delta t$  is given by:

$$\mathbf{y}^{(j)} = \mathbf{y}^n + \Delta t \sum_{k=1}^{j-1} \tilde{a}_{jk} \mathbf{s}(\mathbf{y}^{(k)}, t + \tilde{c}_k \Delta t) + \Delta t \sum_{l=1}^j a_{jl} \mathbf{f}(\mathbf{y}^{(l)}, t + c_l \Delta t), \quad j = 1, \nu,$$

$$\mathbf{y}^{n+1} = \mathbf{y}^n + \Delta t \sum_{j=1}^{\nu} \tilde{\omega}_j \mathbf{s}(\mathbf{y}^{(j)}, t + \tilde{c}_j \Delta t) + \Delta t \sum_{j=1}^{\nu} \omega_j \mathbf{f}(\mathbf{y}^{(j)}, t + c_j \Delta t)$$

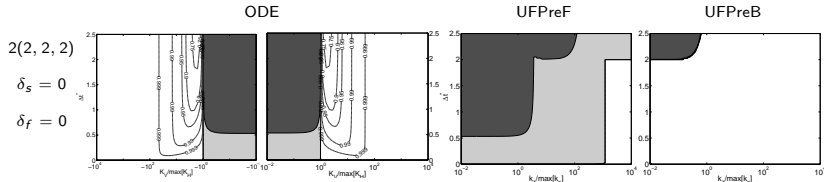
or by the double Butcher tableau:

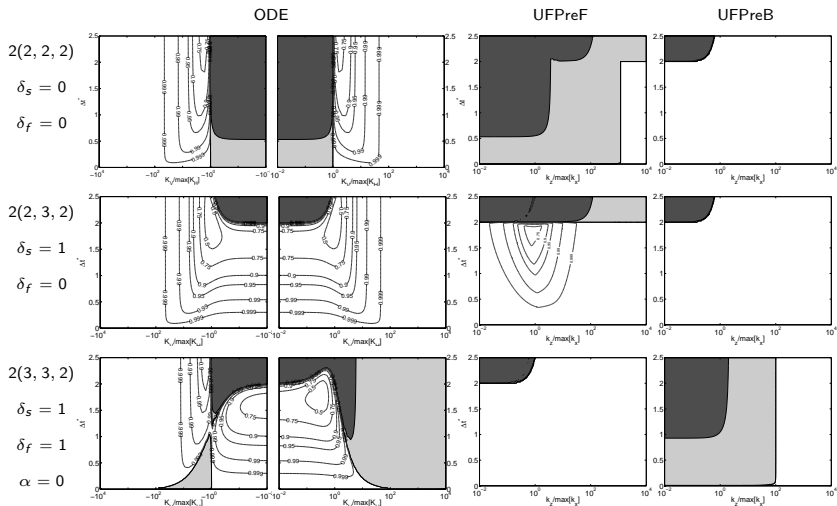
$\tilde{c}_1$	$\tilde{a}_{11}$	$\cdots$	$\tilde{a}_{1\nu}$	$c_1$	$a_{11}$	$\cdots$	$a_{1\nu}$
$\vdots$	$\vdots$	$\vdots$	$\vdots$	$\vdots$	$\vdots$	$\vdots$	$\vdots$
$\tilde{c}_\nu$	$\tilde{a}_{\nu 1}$	$\cdots$	$\tilde{a}_{\nu \nu}$	$c_\nu$	$a_{\nu 1}$	$\cdots$	$a_{\nu \nu}$
	$\tilde{\omega}_1$	$\cdots$	$\tilde{\omega}_\nu$		$\omega_1$	$\cdots$	$\omega_\nu$

Trap2(2 +  $\delta_f$ , 2 +  $\delta_s$ , 2)  
 based on ENDGame formulation (T. Allen)

0	0	0	0	0	0	0	0	0	0
$\delta_s$	$\delta_s$	0	0	0	$\delta_f$	$\delta_f \left(\frac{1-\alpha}{2}\right)$	$\delta_f \left(\frac{1+\alpha}{2}\right)$	0	0
1	$\frac{1}{2}$	$\frac{1}{2}$	0	0	1	$\frac{1}{2}$	0	$\frac{1}{2}$	0
1	$\frac{1}{2}$	0	$\frac{1}{2}$	0	1	$\frac{1}{2}$	0	0	$\frac{1}{2}$
	$\frac{1}{2}$	0	$\frac{1}{2}$	0		$\frac{1}{2}$	0	0	$\frac{1}{2}$

where  $\delta_s, \delta_f = 0, 1$

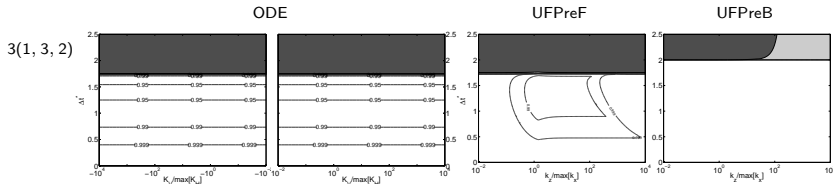




## UJ3(1, 3, 2)

"Strang carryover" scheme (Ullrich and Jablonowski, 2012)

$$\begin{array}{c|ccc|ccc|c}
 0 & 0 & & & 0 & 0 & & & \\
 0 & 0 & 0 & & \frac{1}{2} & \frac{1}{2} & 0 & & \\
 1 & 0 & 1 & 0 & \frac{1}{2} & \frac{1}{2} & 0 & 0 & \\
 \frac{1}{2} & 0 & \frac{1}{4} & \frac{1}{4} & 0 & 0 & 0 & 0 & \\
 1 & 0 & \frac{1}{6} & \frac{1}{6} & 0 & 0 & 0 & 0 & \\
 1 & 0 & \frac{1}{6} & \frac{1}{6} & 0 & 0 & 0 & 0 & \frac{1}{2} \\
 \hline
 & 0 & \frac{1}{6} & \frac{1}{6} & \frac{2}{3} & 0 & 0 & & \frac{1}{2}
 \end{array}$$





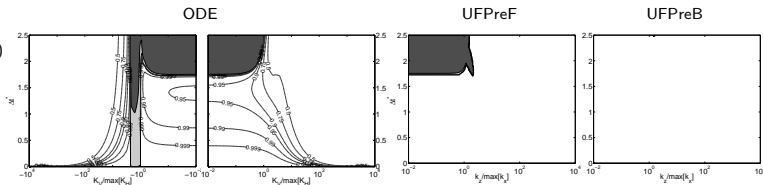
## SSP3(3, 3, 2)

from Pareschi and Russo (2005)

$$\begin{array}{c|ccc|c|ccc}
 0 & 0 & & & \gamma & & & \\
 1 & 1 & 0 & & 1 - \gamma & 1 - 2\gamma & \gamma & \\
 \frac{1}{2} & \frac{1}{4} & \frac{1}{4} & 0 & \frac{1}{2} & \frac{1}{2} - \gamma & 0 & \gamma \\
 \hline
 & \frac{1}{6} & \frac{1}{6} & \frac{2}{3} & & \frac{1}{6} & \frac{1}{6} & \frac{2}{3} \\
 \end{array}$$

$\gamma = 1 - 1/\sqrt{2}$

3(3, 3, 2)



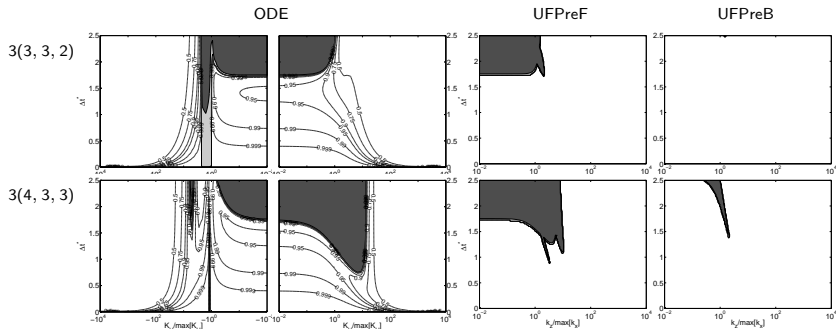


0	0	$\gamma$	$\gamma$	
1	1	$1 - \gamma$	$1 - 2\gamma$	$\gamma$
$\frac{1}{2}$	$\frac{1}{4}$	$\frac{1}{4}$	0	$\gamma$
$\frac{1}{6}$	$\frac{1}{6}$	$\frac{2}{3}$		$\frac{2}{3}$

$\gamma = 1 - 1/\sqrt{2}$

0	0	$\alpha$	$\alpha$	
0	0	0	$-\alpha$	$\alpha$
1	0	1	0	$1 - \alpha$
$\frac{1}{2}$	0	$\frac{1}{4}$	$\frac{1}{4}$	$\delta$
$\frac{1}{6}$	$\frac{1}{6}$	$\frac{2}{3}$	$\frac{1}{6}$	$\frac{2}{3}$

$\alpha = 0.24169426078821$ ,  $\beta = 0.06042356519705$   
 $\eta = 0.12915286960590$ ,  $\delta = \frac{1}{2} - \beta - \eta - \alpha$



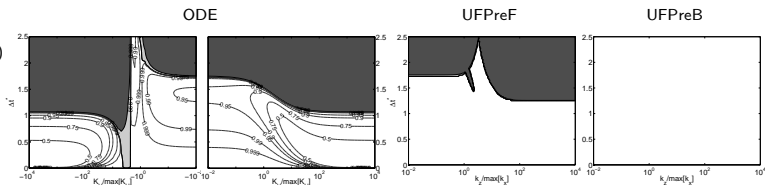


## ARK2(2, 3, 2)

from Giraldo et al. (2012)

$$\begin{array}{c|ccc}
 0 & 0 & & \\
 2 - \sqrt{2} & 2 - \sqrt{2} & 0 & \\
 \hline
 1 & 1 - a_{32} & a_{32} & 0 \\
 \hline
 & \frac{1}{\sqrt{2}} & \frac{1}{\sqrt{2}} & 1 - \frac{1}{\sqrt{2}} \\
 & a_{32} = 1/4 & & 
 \end{array}
 \quad
 \begin{array}{c|ccc}
 0 & 0 & & \\
 2 - \sqrt{2} & 1 - \frac{1}{\sqrt{2}} & 1 - \frac{1}{\sqrt{2}} & \\
 \hline
 1 & \frac{1}{\sqrt{2}} & \frac{1}{\sqrt{2}} & 1 - \frac{1}{\sqrt{2}} \\
 \hline
 & \frac{1}{\sqrt{2}} & \frac{1}{\sqrt{2}} & 1 - \frac{1}{\sqrt{2}} \\
 & \gamma = 1 - 1/\sqrt{2} & & 
 \end{array}$$

3(3, 3, 2)



## Non-linear near-hydrostatic test case (Durrán and Blossey, 2012)

- Equations: non-linear Boussinesq vertical-slice
- Localized forcing ( $\nabla \times \psi$ ) generating gravity waves in stratified shear flow

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- Set-up:

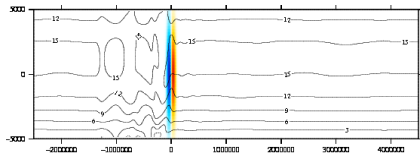
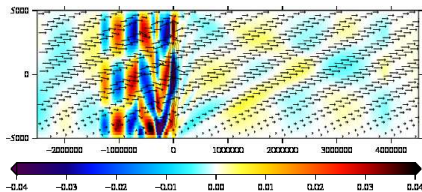
$$u_0(z) = 5 + z + 0.4(5 - z)(5 + z) \text{ m s}^{-1}$$

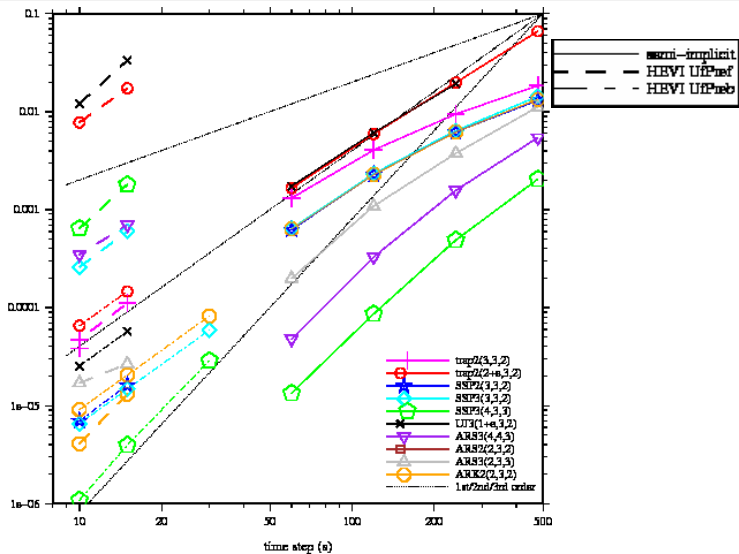
$$\psi(x, z, t) = \psi_0 \left( \frac{\pi x}{L_x} \right) \sin(\omega t) \exp \left[ - \left( \frac{\pi x}{L_x} \right)^2 - \left( \frac{\pi z}{L_z} \right)^2 \right] \text{ m}^2 \text{ s}^{-1}$$

$$\omega = 1.25 \times 10^{-4} \text{ s}^{-1}, L_x = 160 \text{ km}, L_z = 10 \text{ km}, \psi_0 = 10 \text{ m}^2 \text{ s}^{-1}$$

$$\Delta x = 10 \text{ km}, \Delta z = 250 \text{ m}$$

## Non-linear near-hydrostatic test case (Durrant and Blossey, 2012)





## Summary

- Most HEVI schemes performed well in one of UFPref or UFPReB
- Some schemes indicate loss of accuracy moving from semi-implicit to HEVI: SSP3(4,3,3) and ARS\*
- UJ3(1, 3, 2) performs well with only a single implicit solve
- ARK2(2,3,2) shows good error properties & in both UFPref and UFPReB formulations



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## Additionally:

- Here, only stability properties, i.e.  $|A|_{\max}$  from  $A = |A| e^{-i\tilde{K}\Delta t}$
- Also considering  $\tilde{K}\Delta t$  — phase and group velocity properties
- And errors accumulated over  $\Delta t_{\text{SI}} = M\Delta t_{\text{HEVI}}$  for  $M \sim 10$

$$\Rightarrow A^M = |A|^M e^{-iM\tilde{K}\Delta t}$$

Thanks for your attention!

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